Amendments to the Specification:

Please replace the paragraph beginning on page 2, line 18 with the following amended paragraph:

On the other hand, with respect to having a greater glass inside temperature difference between the surface layer and the inner layer upon quenching, it can be explained by the concept of making Biot's number greater. ~~Biot's number is a dimensionless number represented by ((heat transfer coefficient)x(plate thickness)/(heat conductivity)). It is possible to increase the glass tempering degree by making this Biot's number greater.~~ Biot's number is shown by following expression:

$$\beta = h \cdot l / \lambda$$

where β is Biot's number, h is heat transfer coefficient, l is a half of glass thickness and λ is heat conductivity of glass. That is, it is possible to increase the glass tempering degree by having a greater heat transfer coefficient, a greater plate thickness and a less heat conductivity. However, in the case of having a less plate thickness of a tempered glass, that is, in the case of producing a thin plate tempered glass, since heat conductivity of glass is constant in general, it is necessary to make heat transfer coefficient greater in order to make the numerator of Biot's number greater. Therefore, in the case of producing a thin glass plate, a method of making heat transfer coefficient greater is a main countermeasure.

Please replace the paragraph beginning on page 5, line 20 with the following amended paragraph:

In view of the above-mentioned problems, the present invention provides a thin-plate tempered glass, its tempering process and tempering apparatus under a new concept. That is, the present invention provides, in case that a thermally tempered glass is produced by allowing an impact jet flow from a quenching nozzle to blow against the glass, a process for producing a curved, thermally tempered glass, in which the impact jet flow is an underexpansion jet flow and in which a quenching is conducted by simultaneously using at least two types of quenching nozzles having different exit diameters of the quenching nozzles.

Please replace the paragraph beginning on page 8, line 19 with the following amended paragraph:

The quenching nozzles are connected with a chamber generally called a blast head. ~~Upstream of the chamber~~ As an air supply to chamber, a compressor or high-pressure blower is provided. It is preferable that the pressure P of the chamber connected to the quenching nozzles is from 0.1MPa to 0.8MPa. If the pressure P of the chamber connected to the quenching nozzles is lower than 0.1MPa, it is difficult to obtain a thermally tempered glass of a thickness of 2.5mm or less. On the other hand, it is difficult to obtain a pressure exceeding 0.8Pa by a normal apparatus, resulting in a large cost increase. Preferably it is from 0.2MPa to 0.75MPa.